

N F P A

# Fluid Power

VEHICLE

# Challenge



NFPA  
Education and  
Technology  
Foundation

Final Presentation  
University of Denver  
Kevin Lingenfelter  
March 12, 2018



UNIVERSITY of  
DENVER

DANIEL FELIX RITCHIE SCHOOL OF  
ENGINEERING & COMPUTER SCIENCE

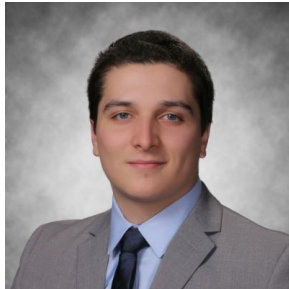
# Agenda

- Team Introductions
- Problem Statement & Objectives
- Current Design
- Summary of Midway Review
  - Design objectives
  - Vehicle design
  - Fluid power circuit design
  - Selection of hardware
  - Results and incorporation of analyses (e.g., finite element analysis)
- Vehicle Testing

# Team Introductions



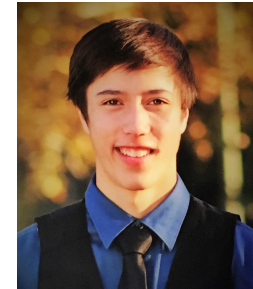
**Matt Imrich**  
Lead CAD Engineer



**Jason McLean**  
Lead Test Engineer



**Ryan Ortiz**  
Financial Manager  
Head of Research



**Kyle Sun**  
Co-Project Manager  
Lead Technical  
Writer



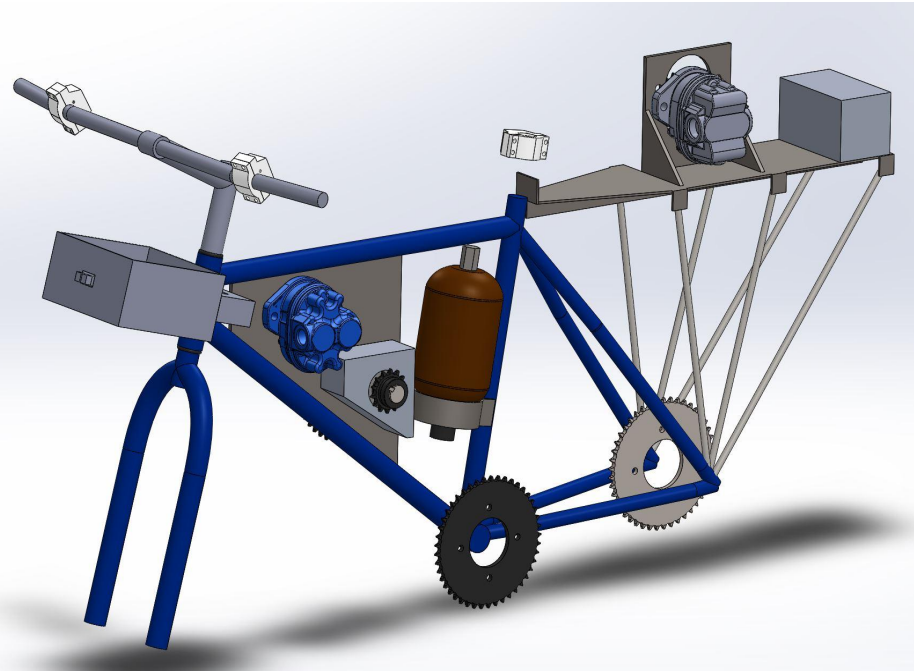
**Emma Willis**  
Co-Project Manager  
Lead Systems  
Engineer

# Problem Statement and Objectives

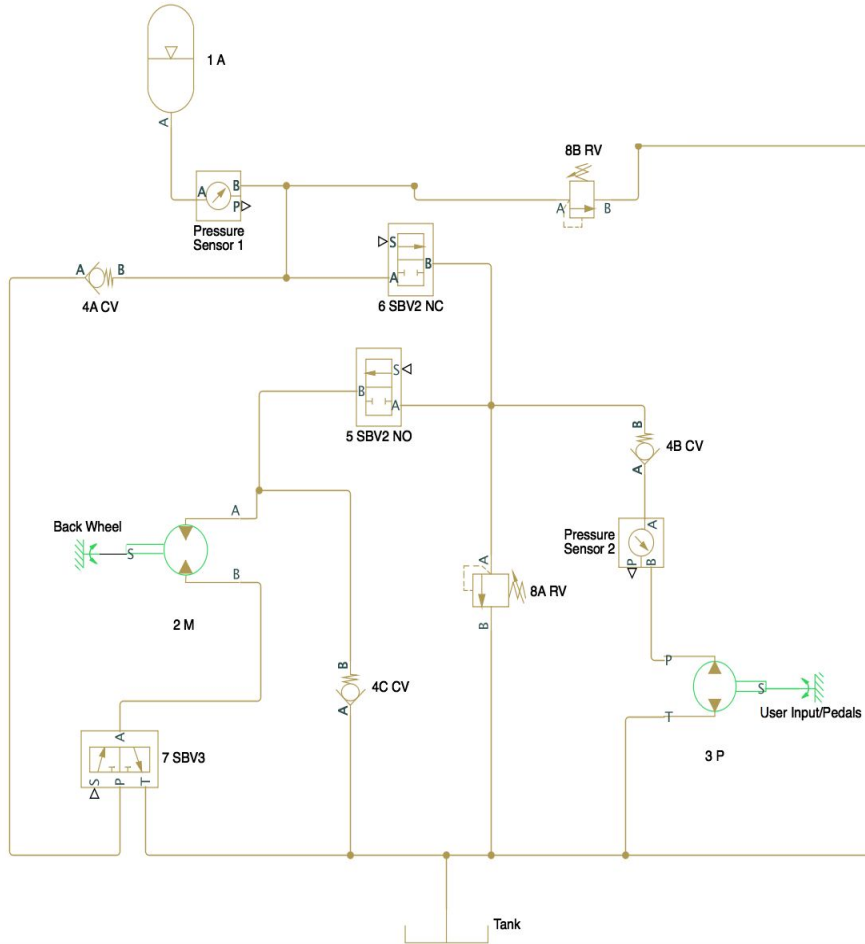


- **Problem Statement:** This project requires the design and construction of a single-rider vehicle that uses a fluid power system involving energy storage and regeneration technology
- The objectives of this project include:
  - Design
  - Analysis
  - Fabrication
  - Competition
- The requirements for the project are based on the NFPA FPVC rules and regulations.

# Final Vehicle



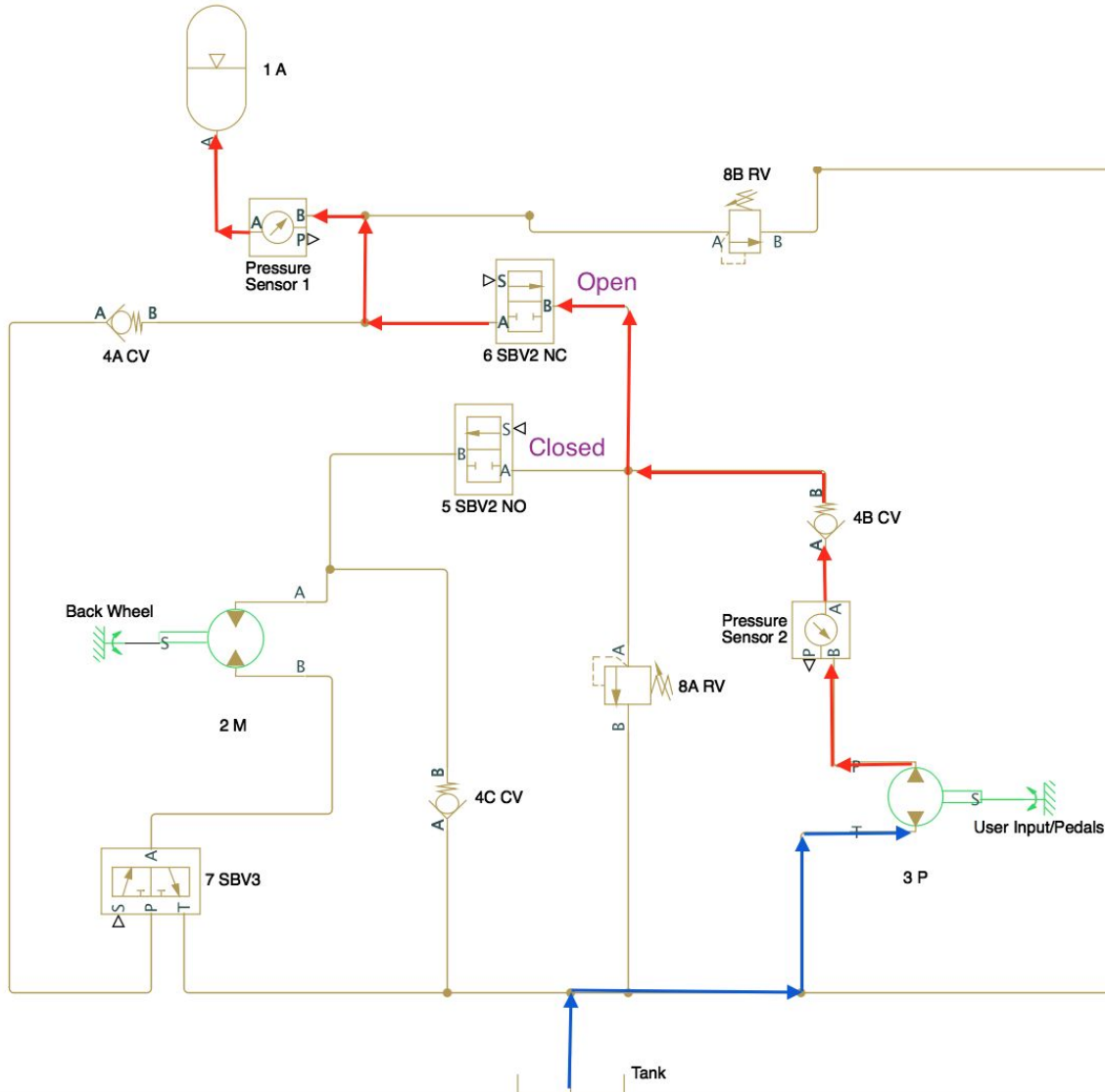
# Fluid Power Circuit Design





Bill of Materials		
Item No.	Description	Quantity
1	1 quart accumulator	1
2	0.54 CID Motor	1
3	0.5 CID Pump	1
4	Check Valve	3
5	2 way solenoid valve (normally open)	1
6	2 way solenoid valve (normally closed)	1
7	3 way solenoid valve	1
8	Pressure Relief Valve	2

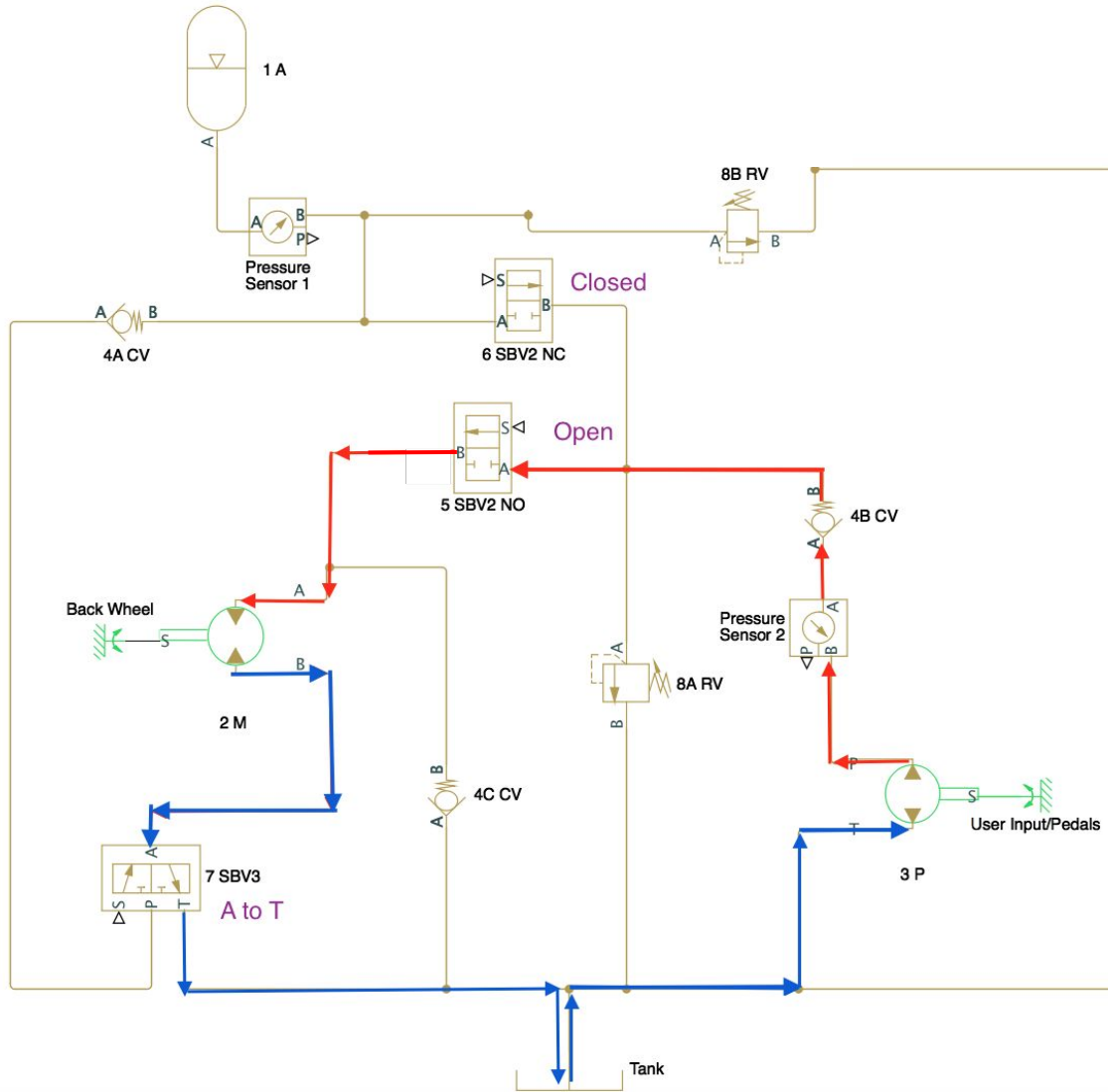
Key	
High Pressure Line	
Low Pressure Line	



# Precharge Circuit



Key	
High Pressure Line	
Low Pressure Line	

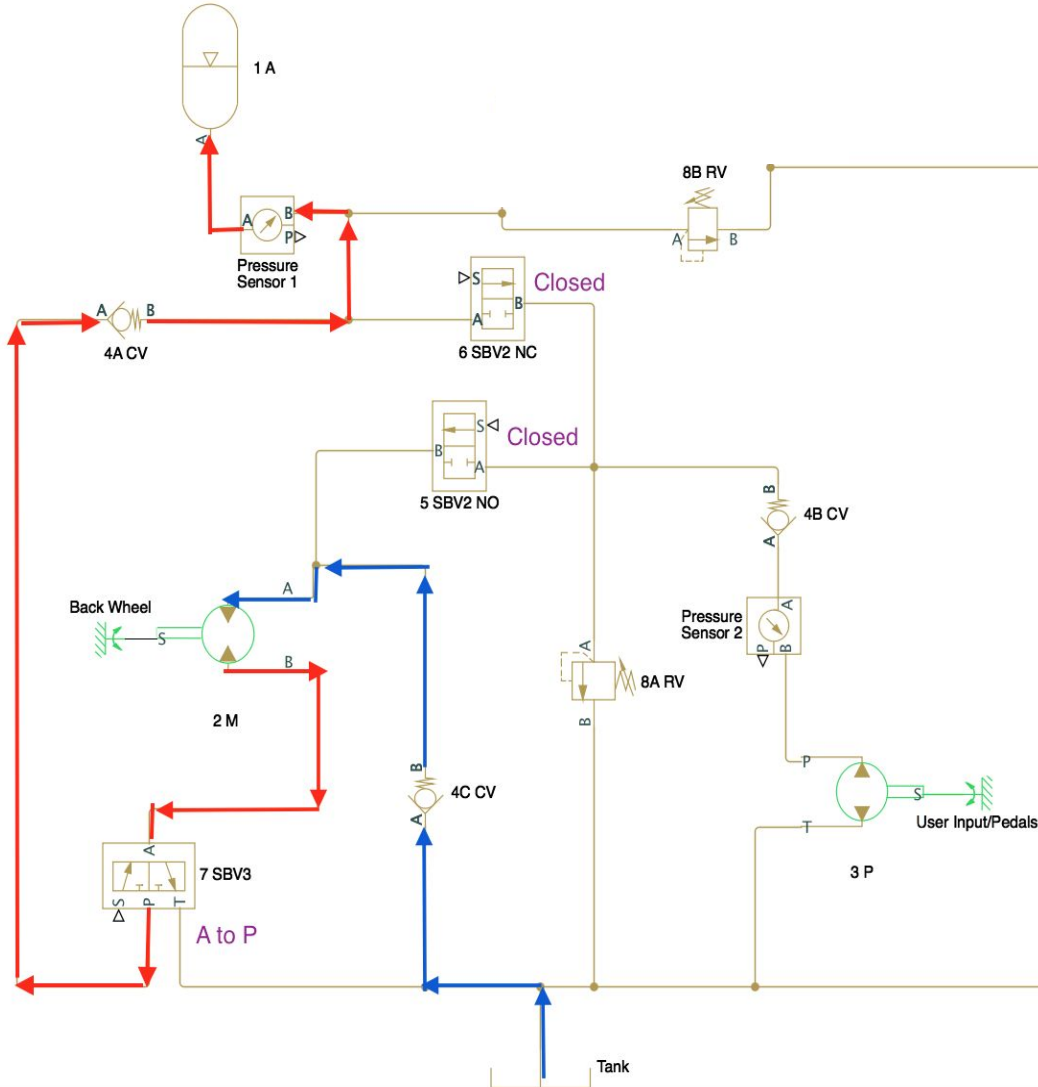
# Driving Circuit





Key	
High Pressure Line	
Low Pressure Line	

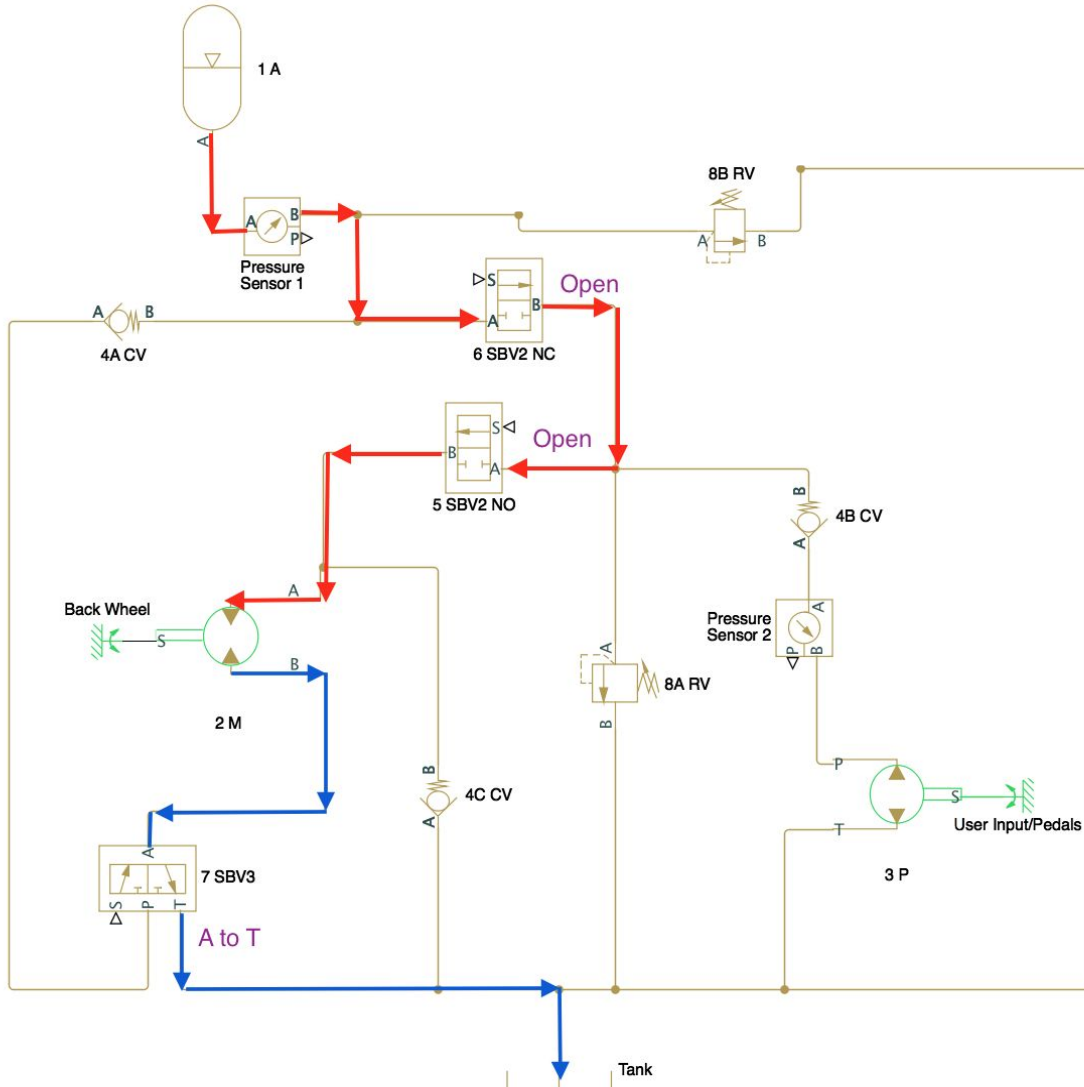




# Regeneration Circuit



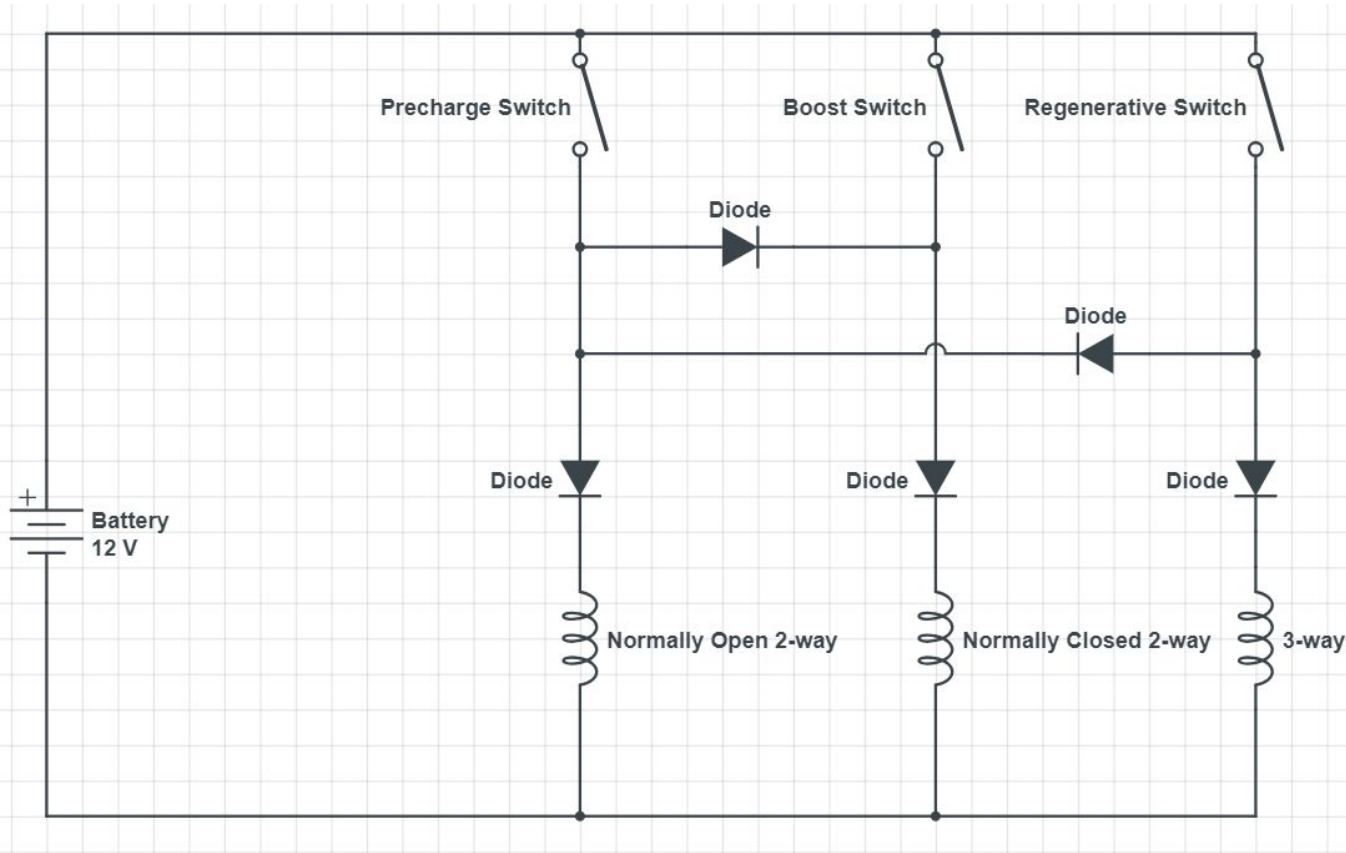
Key	
High Pressure Line	
Low Pressure Line	

# Boost Circuit



Key	
High Pressure Line	
Low Pressure Line	

# Electronic Circuit



Mode	V5	V6	V7
Precharge	1	1	-
Boost	0	1	0
Drive	0	0	0
Regenerative	1	0	1

# Hardware Selection



## Accumulator:

- Accumulators, Inc.
- A1QT3100-3
- 1 Quart
- Bladder
- Rated for 3000 psi



## Pump

- Eaton 26002-RZG
- 0.5 CID
- Clockwise rotation



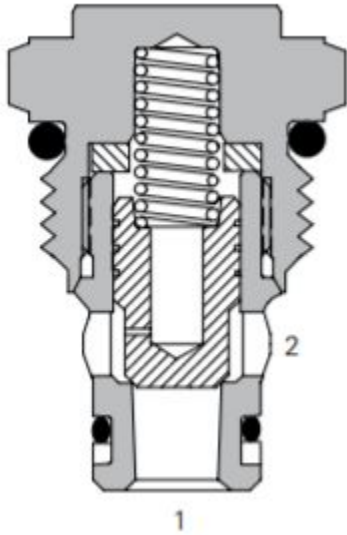
## Motor:

- Eaton 26702-DAB
- 0.54 CID
- .625" Keyed shaft
- Bi-rotation
- Internal drain

# Hardware Selection

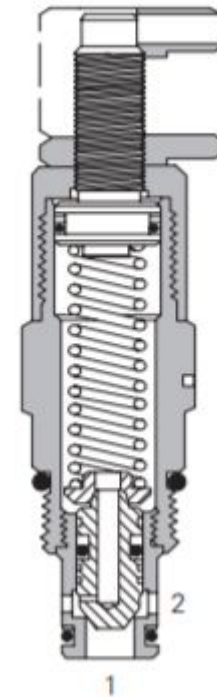
## CV3-8 Check Valve (3):

- Application pressure 5000 psi
- Valve remains closed until spring bias is reached at port 1, lifting poppet and allows flow from 1-2
- Hardened steel ball limits leakage and extends service life

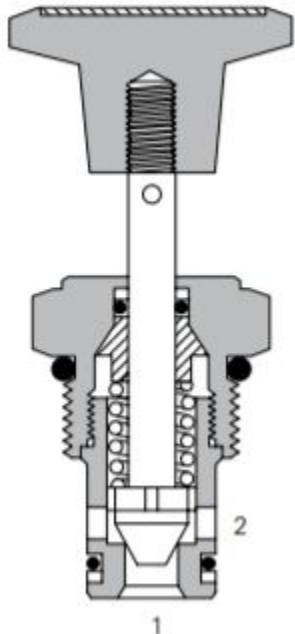


## RV1-10 Relief Valve (2):

- Application pressure 3000 psi
- Direct acting
- Remains closed until predetermined setting is reached at port 1
- Fast acting, low pressure rise
- Low internal leakage, high flow rate



# Hardware Selection

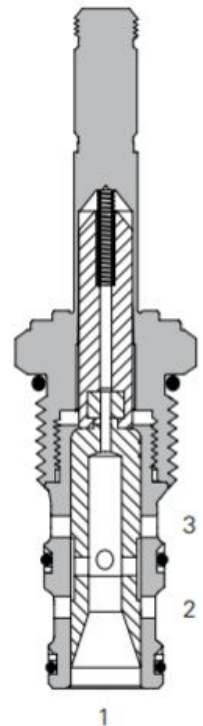


## NV1-8 Flow Restrictor Valve (1):

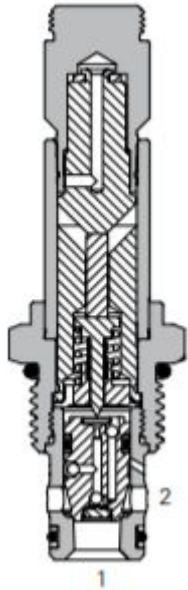
- Application pressure 5000 psi
- Needle valve that cause a pressure drop as it passes from port to port
- Adjustable pressure selection through rotation of the screw

## SV1-10 3-way Solenoid Valve (1):

- Application pressure 3000 psi
- When de-energized, allows flow from 1-2 while port 3 is blocked
- When energized, allows flow from 3-1 while port 2 is blocked
- Low leakage, compact design



# Hardware Selection

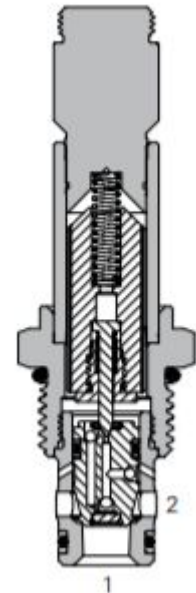


## SBV11-10-O 2-way Solenoid Valve (1):

- Application pressure 5000 psi
- Normally open
- When de-energized, valve is open for full flow in both directions
- When energized, pilot poppet closes causing main poppet to close
- Low leakage, compact design

## SBV1-10-C 2-way Solenoid Valve (1):

- Application pressure 3000 psi
- Normally closed, bi-directional
- When de-energized, valve is blocked in both directions
- When energized, pilot poppet is released allowing main poppet to open allowing flow in both directions
- Low leakage, compact design



# Analysis



Road Grade	7%
Weight (Vehicle + Rider)	300 lbs
Rolling Resistance (Bike Tire on Rough Road)	0.008
Tire Radius	13 in
System Pressure	1000 psi
Motor Efficiency	0.9
Pump Efficiency	0.95
Bike Speed	10 mph
Fluid Velocity	20 ft/s
Pedal Rate (RPM)	60



# Motor and Pump Sizing

	Motor	Pump
Required CID	2.1185	4.8972
Selected CID	0.54	0.5
Required Mechanical Advantage	4	10
RPM	129.2308	600
GPM	1.2084	1.2987

# Tube Sizing

	Tube
Fluid Velocity	20 ft/s
Required Diameter	0.1569 in
Selected Diameter	0.25 in (0.375 in)



# Pipe Calculations

- S = Allowable Stress → S = 8000 psi (Aluminum 6061)
- E = Quality Factor → E = 1 (Seamless)
- t = Wall Thickness → t = .091 in
- C = Depth of Thread → C = 0 (Not Threaded – Welded)
- D = Nominal Outer Diameter → D = 3/8 in

P = Working Pressure

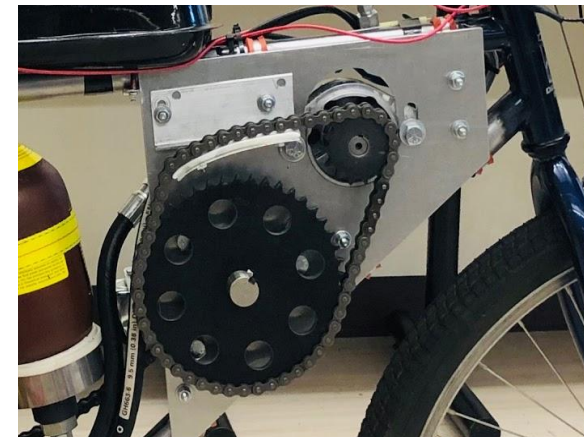
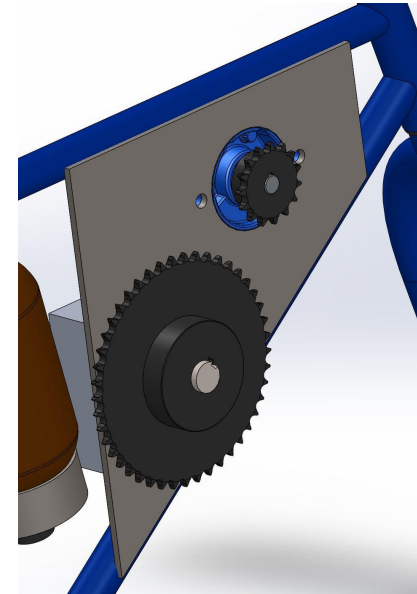
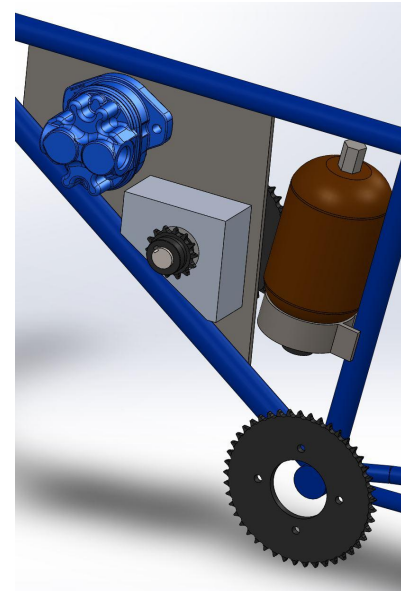
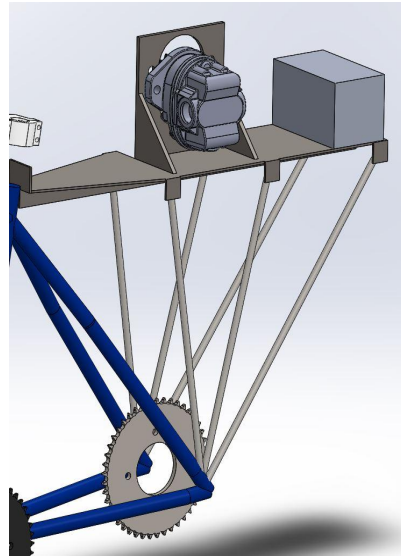
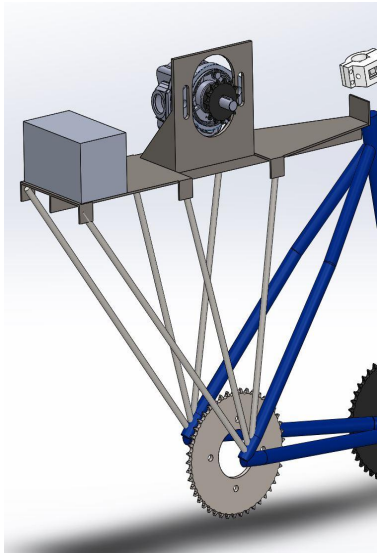
$$P = \frac{2 * SE(t - C)}{D}$$

$$P = \frac{2 * 8000 \text{ psi} (1.0)(.091 \text{ in} - 0 \text{ in})}{\frac{3}{8} \text{ in}}$$

$$P = 3882.67 \text{ psi}$$

$$\text{Safety Factor} = 3882.67 \text{ psi} / 3000 \text{ psi} \sim 1.3$$

# Mounting

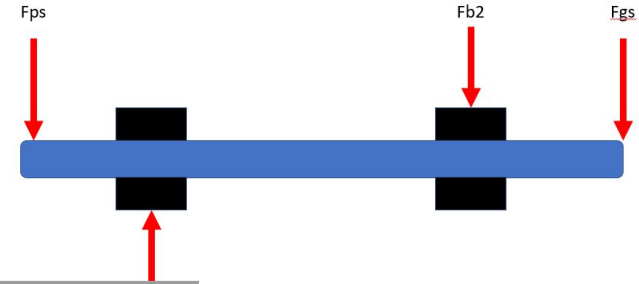


# Bearing Analysis

$$L_p = K_R \left(\frac{C}{P}\right)^3 \quad C = P^3 \sqrt{L_5 / K_R}$$

For 800 hrs operation at 200 rpm → L~10 million cycles

5% Failure Rate →  $K_R = 0.62$



## Loading/Life Limitations

	Worst Case (P = 3000 psi)	Normal Operation (P = 1000 psi)
$C_1$	1307.86 lbs	271.40 lbs
$C_2$	792.96 lbs	90.71 lbs
$L_1$	2.46 million cycles	275.8 million cycles
$L_2$	11.06 million cycles	7387.34 million cycles



Purchased Bearings:  
**C = 820 lbs**

# Shaft Analysis



**Selected Shaft: Stainless Steel 316**

$S_{ut} = 90$  ksi

$S_y = 40$  ksi

D = 1 in, Machined Surface, 99.99% Reliability



	Safety Factor ( $N_f$ )
<b>Worst Case (P = 3000 psi)</b>	2.2669
<b>Normal Operation (P = 1000 psi)</b>	8.1079

$$N_f = \frac{d^3 \pi}{32} \left[ \frac{\sqrt{(K_f M_a)^2 + \frac{3}{4} (K_{fs} T_a)^2}}{S_f} + \frac{\sqrt{(K_{fm} M_m)^2 + \frac{3}{4} (K_{fsm} T_m)^2}}{S_{ut}} \right]^{-1}$$

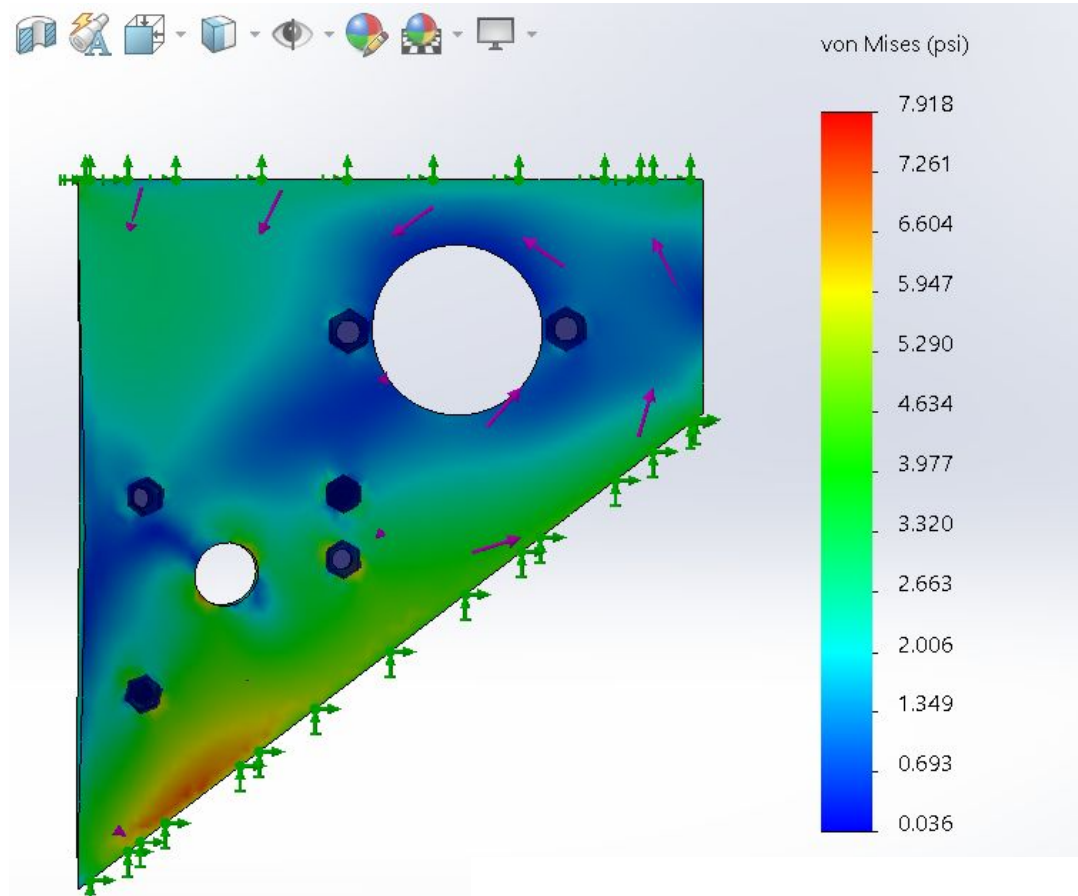
$$S_f = 0.5 * S_{ut} C_{load} C_{size} C_{rel} C_{surf}$$

# Shaft Key Calculations

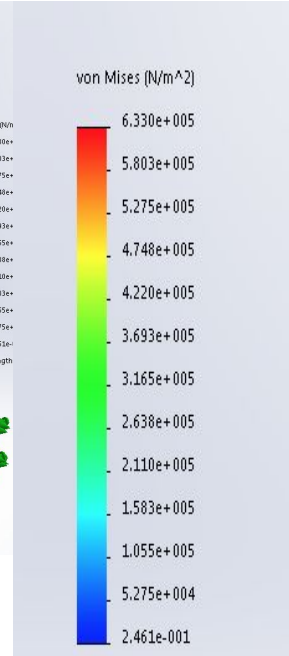
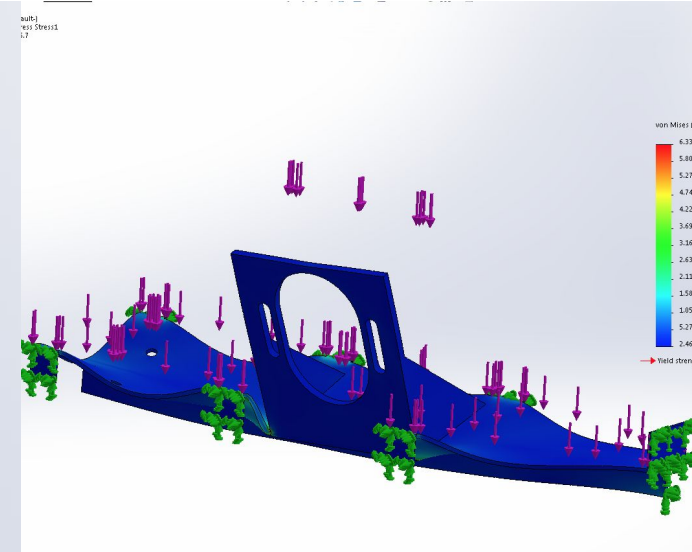
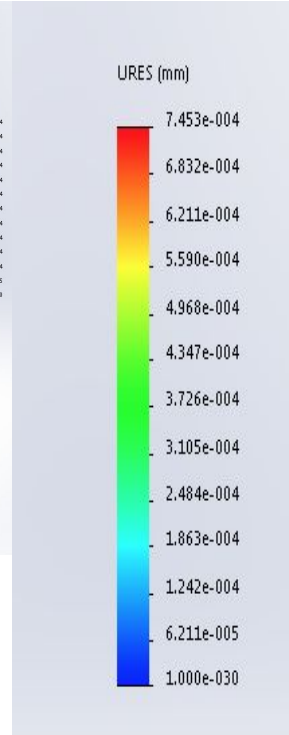
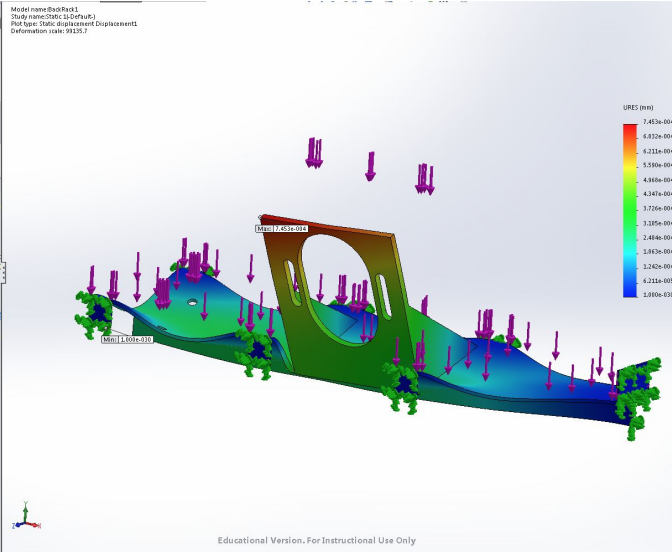
	Pressure	Safety Factor
Large Sprocket Key	3000 psi	22.5
	1000 psi	64
Small Sprocket Key	3000 psi	5.84
	1000 psi	16.64



# Load Analysis



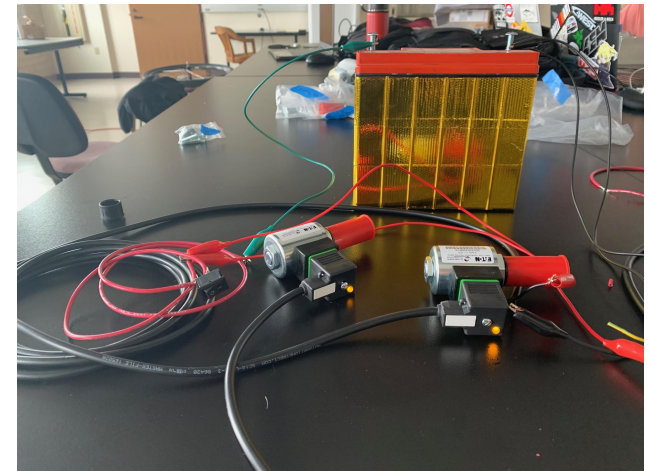
# Detailed design - Rear Gear





# Electronic Verification

Components	Voltage	Peak Current
2-Way Solenoid Valve (Normally Open)	12 V	1.912 A
2-Way Solenoid Valve (Normally Closed)	12 V	1.912 A
3-Way Solenoid Valve	12 V	2.432 A



# Electronic Verification



Components	Voltage	Amperage	Initial Current
EXP1250	12 V	5 A	1.5 A
EXP12180	12 V	18 A	5.4 A

# Weight Verification

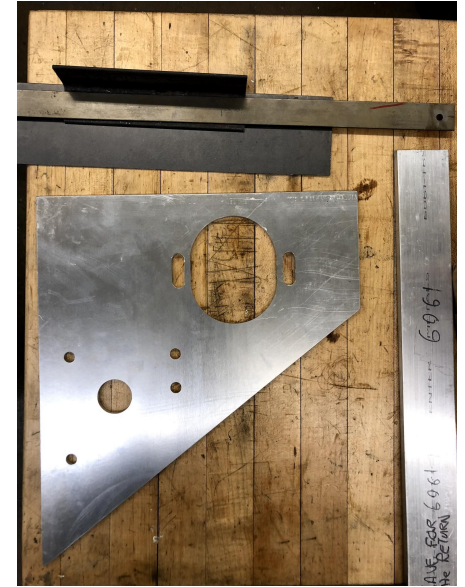
Weight Limit	Current Estimated Weight
210 lbs Excluding Rider Includes Fluid	181 lbs.



Key Components	Weight
Frame	30 lbs
Rear Wheel Assembly	9.8 lbs
Center Plate	1.2 lbs

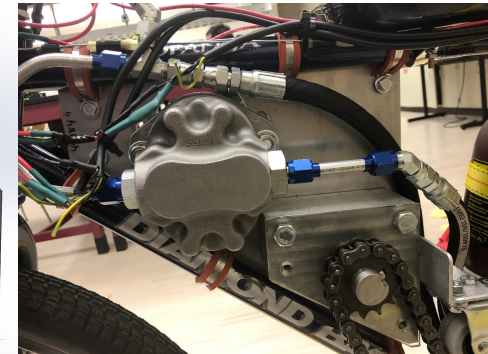
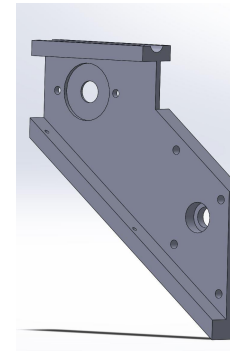
# Construction

N F P A  
**Fluid Power**  
VEHICLE  
*Challenge*

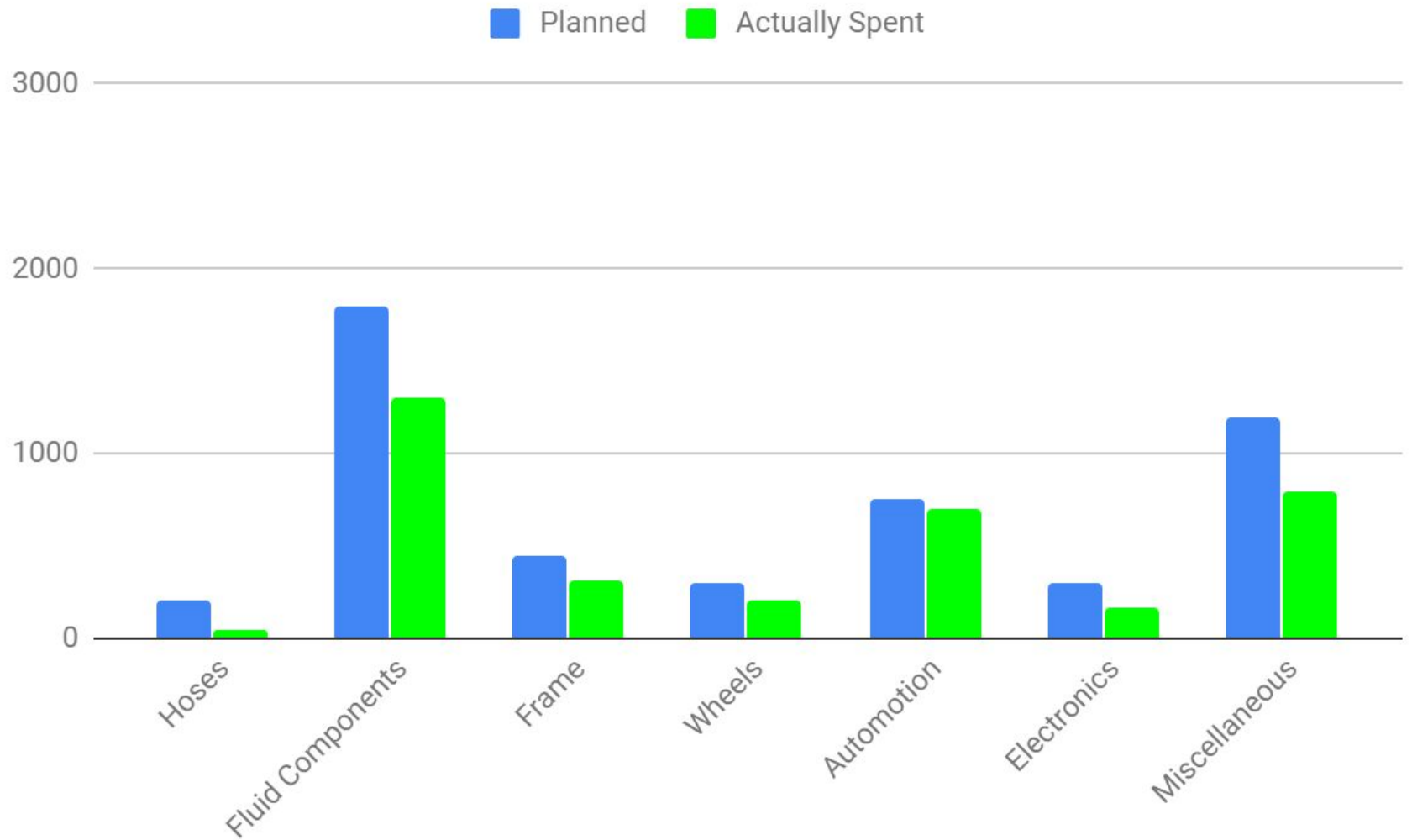


# Key Design Changes

- Battery holder from 3D print to metal
- Center pump mount from u-bolt clamp to steel band hanger clamp
- Back rack from custom design to prefabricated
- New Battery to meet current demands
- Moved motor mount
- Added chain tensioners
- New diodes
- Wider pedal spindle



# Budget Summary



# Lessons Learned

- **Time management**
  - Leave time for unexpected problems and design changes
- **Use the resources available**
  - Others expertise is extremely helpful
- **Delegate tasks early**
  - Keeps the whole team engaged and productive;
- **Balance design objectives**
  - Torque vs speed
  - Weight vs feasibility

# Thank you!



We would like to extend a huge thank you to all the people who helped us

- NFPA, Ernie Parker, Jeff McCarthy, Stephanie Scaccianoce
- Kevin Lingenfelter
- Adam York, Ronald Delyser, Ann Deml
- Hans Green & JILA
- Lucky Bikes Recyclery
- Shane Ware and DU Bike Shop





# Motor Sizing

## Torque Required

$$T = \text{rad} * \text{pull} = 303.4574 \text{ lb-in}$$

## Required Motor CID

$$\text{Disp} = \text{Torque} * 2\pi / (\text{Pressure} * \text{Motor Efficiency}) = 2.1185$$

Motor Selected: 0.54 CID

## Required Mechanical Advantage from Motor to Wheels

$$\text{MA} = \text{required motor CID} / \text{Selected motor CID} = 3.9232 (\sim 4)$$

Wheel RPM Required to Travel 10 mph: 129.2308 rpm

Fluid GPM to Achieve 10 mph:

$$\text{GPM} = \text{MotorCID} * \text{MA} * \text{RPM} / 231 = \underline{1.2084 \text{ gpm}}$$



# Pump Sizing

## Required Pump CID:

$$\text{CID} = (\text{GPM} * 231) / (\text{RPM pedal} * \text{Pump Efficiency}) = 4.8972$$

Pump Selected: **0.5 CID**

## Required Mechanical Advantage for Pedals to Pump:

$$\text{MA} = \text{Required Pump CID} / \text{Selected Pump CID}$$

$$\text{MA} = 9.7943 (\sim \mathbf{10})$$

Pump RPM:  $\text{RPM} = \text{RPM pump} * \text{MA}$

$$\text{RPM} = \mathbf{600}$$

Pump GPM:  $\text{GPM} = \text{RPM pump} * \text{Motor CID} / 231$

$$\text{GPM} = \mathbf{1.2987}$$



# Tubing

## Fluid Velocity

vel = 20 ft/s

**Net Area:**  $A = 0.32 * \text{GPM} / \text{vel}$

$A = 0.0193 \text{ in}^2$

**Required Diameter:**  $D = 2 * \text{sqrt}(A / \pi)$

$D = 0.1569 \text{ in}$

**Selected Diameter:**  $\frac{1}{4} \text{ in.}$

Accommodate Smaller Fluid Velocities:  $\frac{3}{8} \text{ in.}$

**Burst Pressure:**  $P_b = (2 * S_t * t_m) / D$

Using a  $\frac{1}{4}$ -10S Small Pipe

$P_b = (2 * 15000 \text{ psi} * 0.065 \text{ in}) / 0.540 \text{ in}$

$P_b =$  3611.1 psi